

Simultaneous Achievement of High Control Performance and Energy Efficiency of EH Systems

via

Parallel Connection of Pump and Valve Control Units

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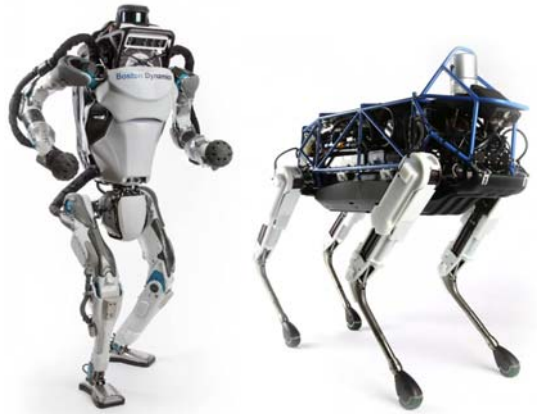
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Outline

- **Motivation**
- **Brand New Hardware Configuration:**
 - Parallel connection of pump and valves*
- **Control Design I**
 - Easy to implement, Feedforward control of the pump*
- **Control Design II**
 - Minimized throttling losses*
- **Conclusions**

Motivation

□ Demand for high performance & high energy efficient electro-hydraulic systems



Hydraulic robots: Atlas & Spot (Boston Dynamics)



Remote-controlled excavator



Heavy-duty manipulator

- **Strict administrative regulations** demand energy consumption and CO₂ emissions reductions for the industry;
- Heating in a hydraulic system causes adverse effects;
- Operating costs would increase in energy-inefficient systems;
- **Energy sources must be carried on board** in mobile robotic systems.

How to achieve objectives of high performance & high energy efficiency simultaneously?

Motivation

■ Valve controlled system

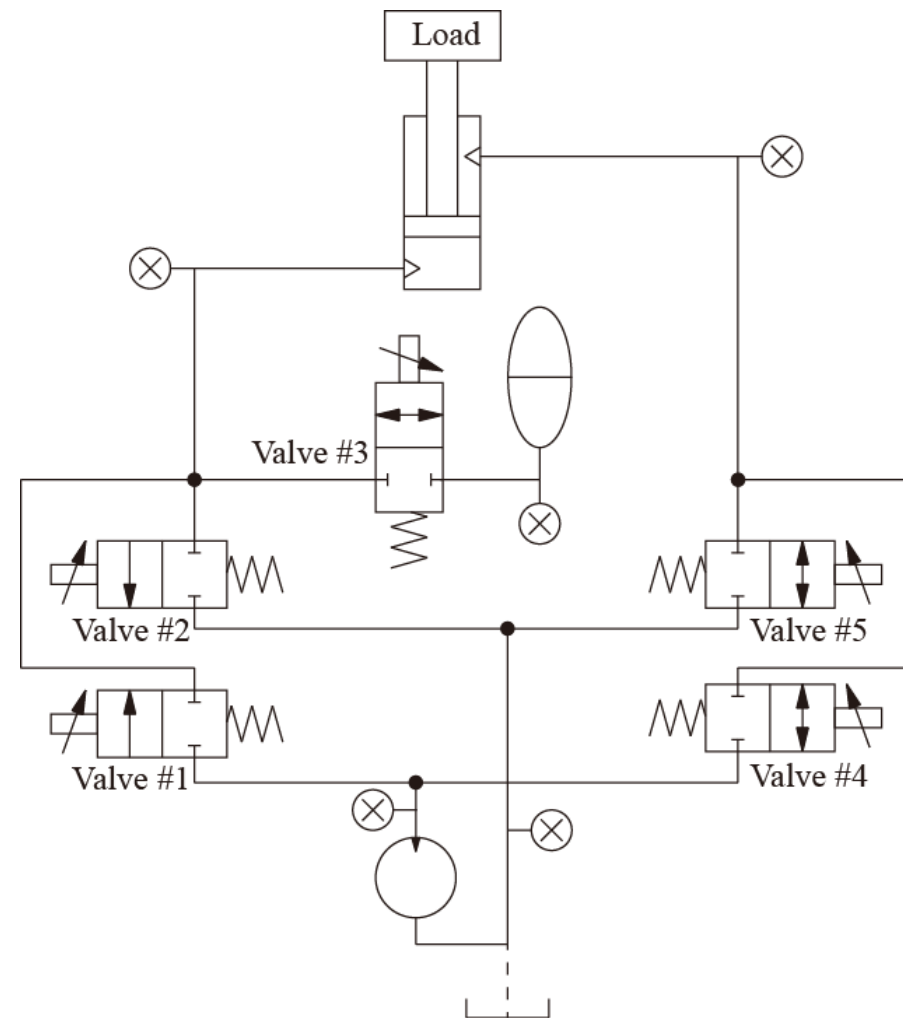
Single valve

Independent meter-in and meter-out

(J-O Palmberg, B. Eriksson, J. Mattila, A Shenouda...)

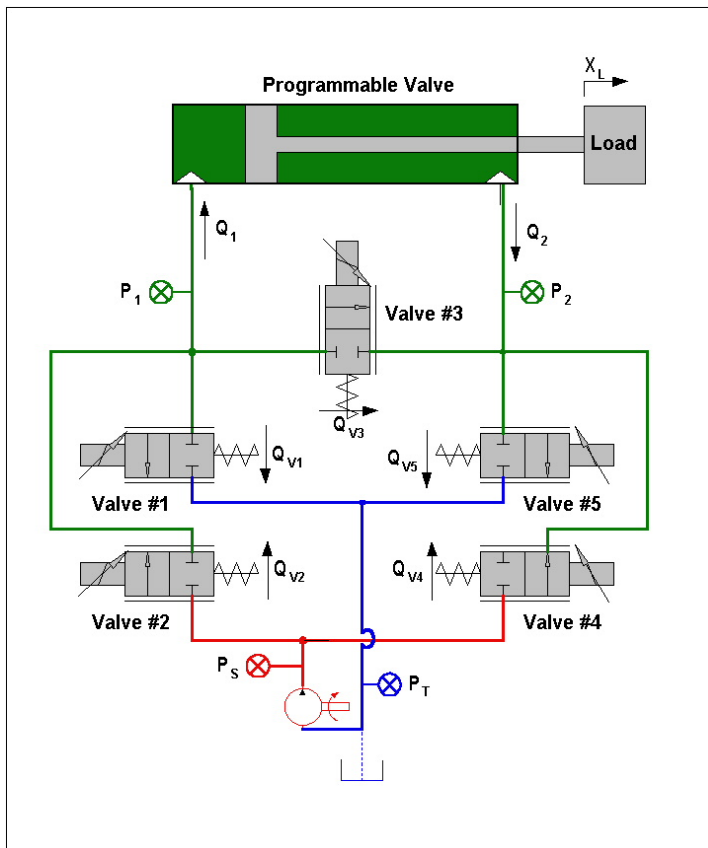
Energy-saving programmable valves with regeneration and energy recovery

(B. Yao, et al, 2000-2012)



INTEGRATED MECHATRONIC DESIGNS

Automated Modeling and Energy Saving Adaptive Robust Control of Electro-Hydraulic Systems with Novel Programmable Valves



Better control performance achieved with cheaper valves and less energy usage!

Motivation

■ *Valve controlled system*

Single valve

Independent meter-in and meter-out

(J-O Palmberg, B. Eriksson, J. Mattila, A Shenouda...)

*Energy-saving programmable valves
with regeneration and energy recovery*

(B. Yao, et al, 2000-2014)

✓ High control performance

**× Unavoidable significant amount of
throttling losses**

Motivation

■ Pump controlled system

Variable displacement or variable speed

(M. Ivantysynova, N. Manring, T. Minav, KK. Ahn, B. Xu...)

✓ *High energy efficiency*

-Generally, lower bandwidth compared to the servo valve

-Improving the pump performance → better control performance

-Asymmetric cylinder

One theme in IFK'2014 in Aachen:

✓ Higher system energy efficiency demands have made pump controlled systems a trend

× Poor control performance due to limited closed-loop bandwidths of pump controlled systems

Motivation

■ Valve controlled system

Single valve

Independent meter-in and meter-out

(J-O Palmberg, B. Eriksson, J. Mattila, A Shenouda...)

Energy-saving programmable valves

(B. Yao...)

✓ High control performance

✗ Large amount of throttling losses

■ Pump controlled system

Variable displacement or variable speed

(M. Ivantysynova, N. Manring, T. Minav, KK. Ahn, B. Xu...)

✓ High energy efficiency

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-Asymmetric cylinder

■ Our idea

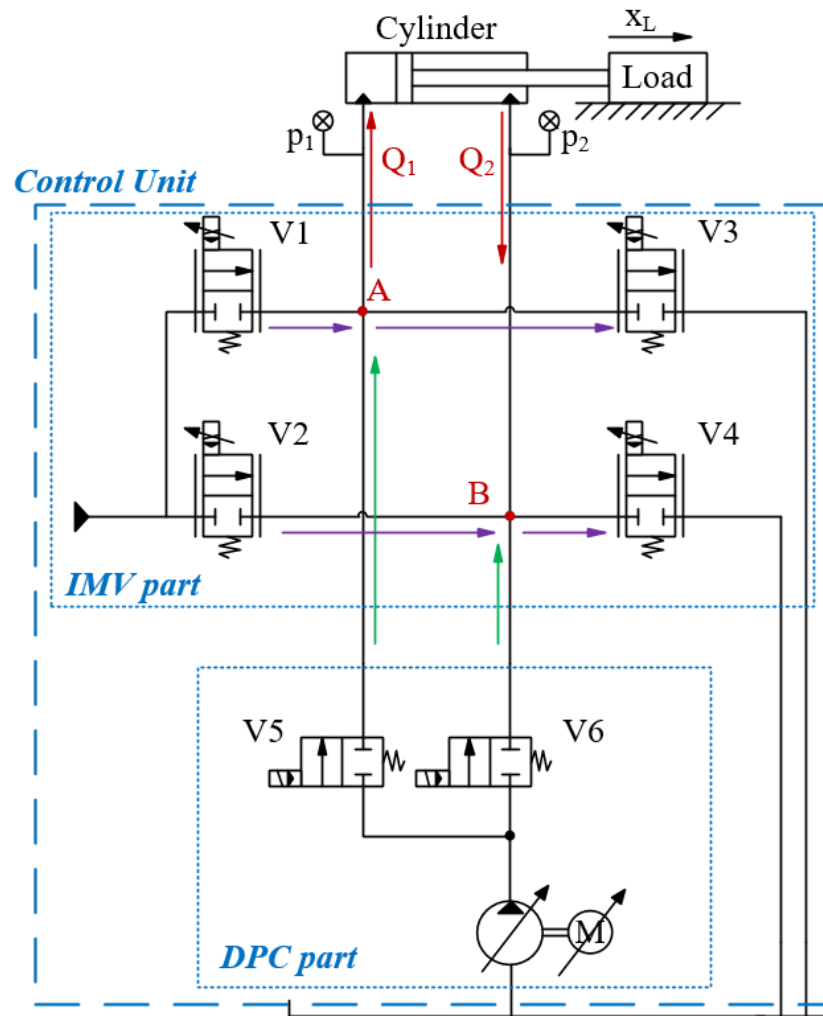
Combining and making full use of benefits of the two different types of control units

parallel connection: independent metering valves & pump

Control performance → *Better valve controlled system*

Energy efficiency → *Pump controlled system*

Hardware Configuration



■ Two main parts:

-Independent metering valves (IMV) part:

-Direct pump control (DPC) part:

■ Parallel connection of pump and valves

-Flow @ point A and B

■ Basic working principles

-Pump provides the majority amount of flow---
energy-efficient

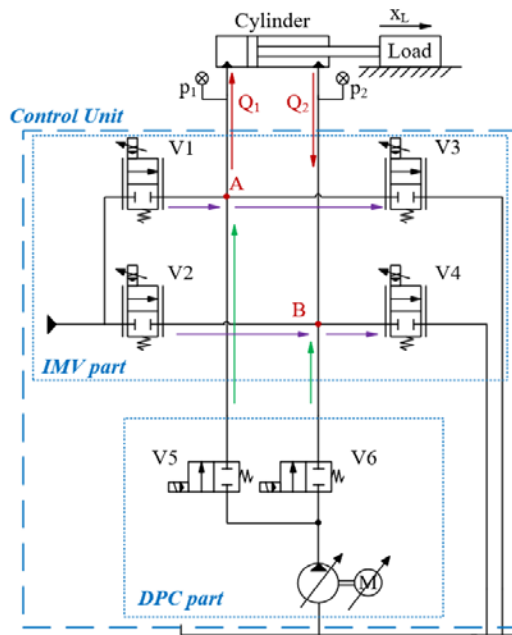
-Valves guarantee tracking performance with
small amount of flow---**high control performance**

Hardware Configuration



Experimental Facilities at the State Key Laboratory of Fluid Power and Mechatronic Systems, Zhejiang University, Hangzhou, China, where I was honored as a Changjiang Chair Professor as well

Control Design



■ Challenges

- parametric uncertainties, uncertain nonlinearities, disturbances...
- flexibilities** brought by the hardware configuration
- relatively poor **dynamic performance of the pump**
- how to **minimize the throttling losses**



- How to control the two parts coordinately to achieve the two objectives simultaneously?

Two control designs will be presented.

Control Design I

■ Relatively poor dynamic performance of the pump in the test rig



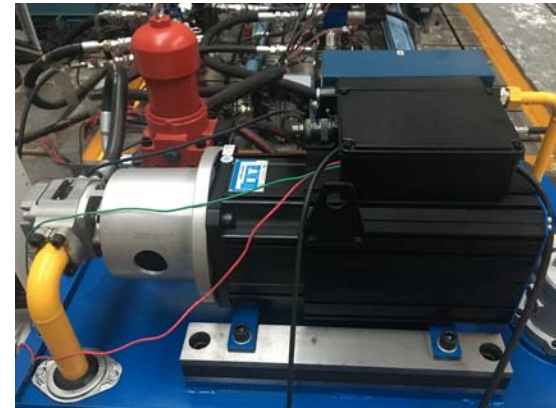
Variable displacement pump

- slow dynamic response
- time-delay
- large outlet compressible volume



time-delay & 2nd order

$$G_{p1}(s) = \frac{Q_{p1}(s)}{u_{p1}(s)} = e^{-\tau_{d1}s} \frac{k_{p1}\omega_n^2}{s^2 + 2\varepsilon\omega_n s + \omega_n^2}$$



Servo-motor pump

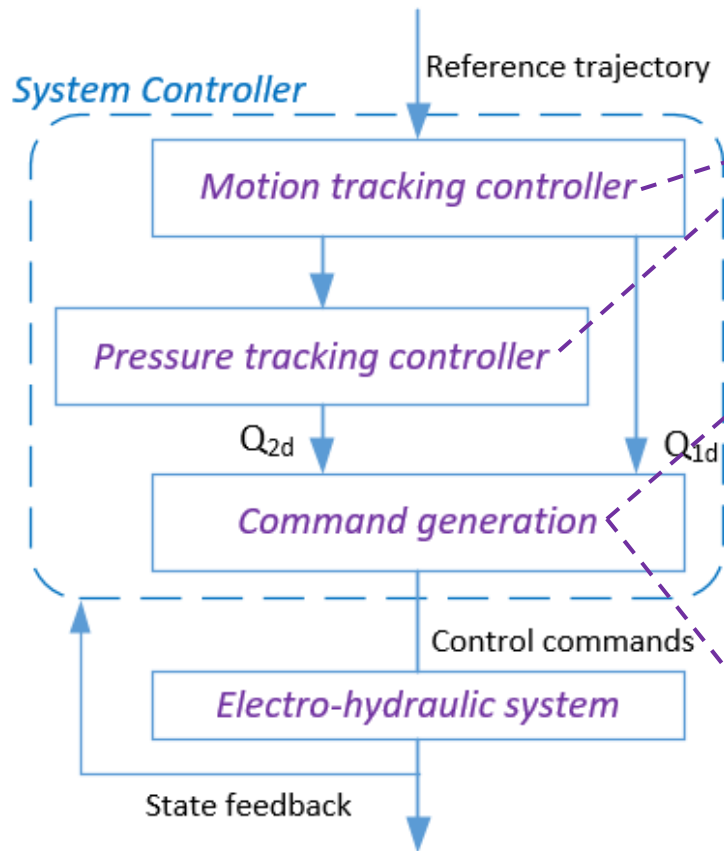
- better, but still not as good as the valve



time-delay & 1st order

$$G_{p2}(s) = \frac{Q_{p2}(s)}{u_{p2}(s)} = e^{-\tau_{d2}s} \frac{k_{p2}}{\tau_n s + 1}$$

Control Design I



- **Desired cylinder flow Q_{1d} and Q_{2d} based on adaptive robust control (ARC) approach**

- **Feedforward control of the pump**

$$u_p(s) = \frac{1}{G_p(s)} Q_{ideal}(s)$$

- to provide the **ideal cylinder flow $Q_{1 ideal} = A_1 \dot{x}_d$ and $Q_{2 ideal} = A_2 \dot{x}_d$**

- no feedback---easy to implement in practice

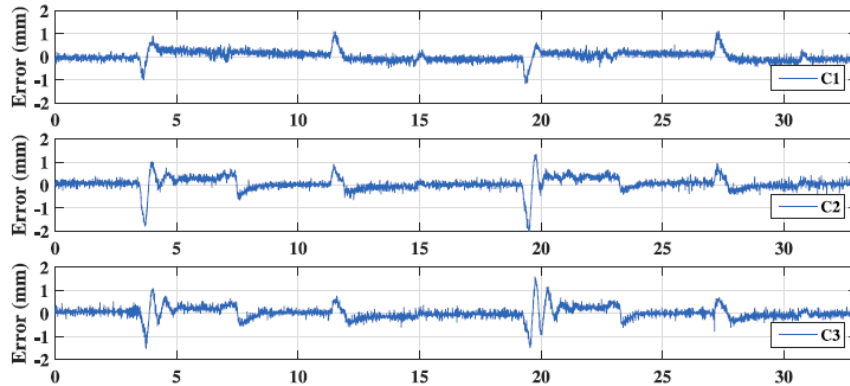
- **Valves control the rest amount of flow**

- differences** between the desired flow Q_{1d} & Q_{2d} and the ideal flow $Q_{1 ideal}$ & $Q_{2 ideal}$

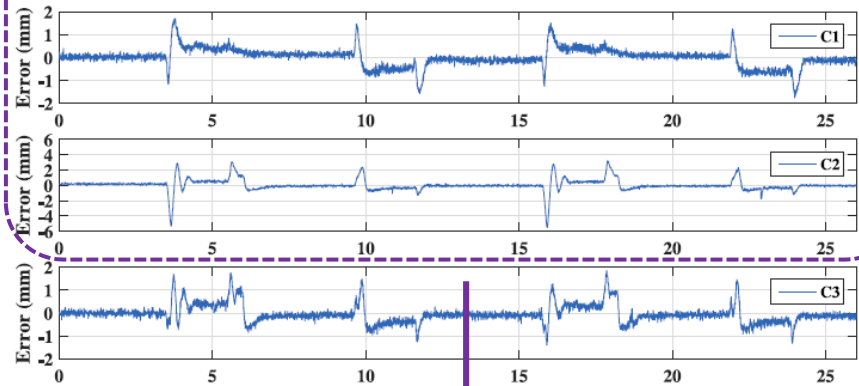
Comparative Experiments with Controller I

- **Tracking performance** (using the variable displacement pump)
 - With (C1) and without (C2) feedforward control of the pump
 - Four-valve independent metering control method (C3)

Low speed & acceleration (0.15m/s , 0.3m/s^2)



High speed & acceleration (0.25m/s , 3m/s^2)

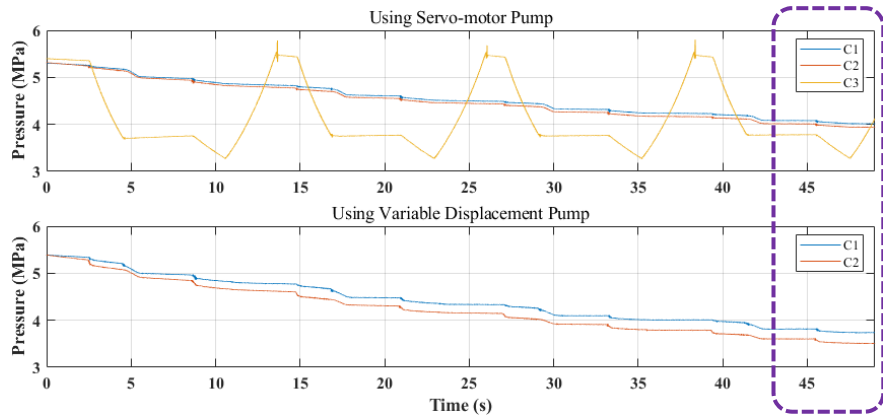


- ✓ Same level of **high tracking performance**: C1 & C3
- ✓ **Effectiveness of the feedforward control method in C1** (such a pump can hardly be used in a precise motion control project)

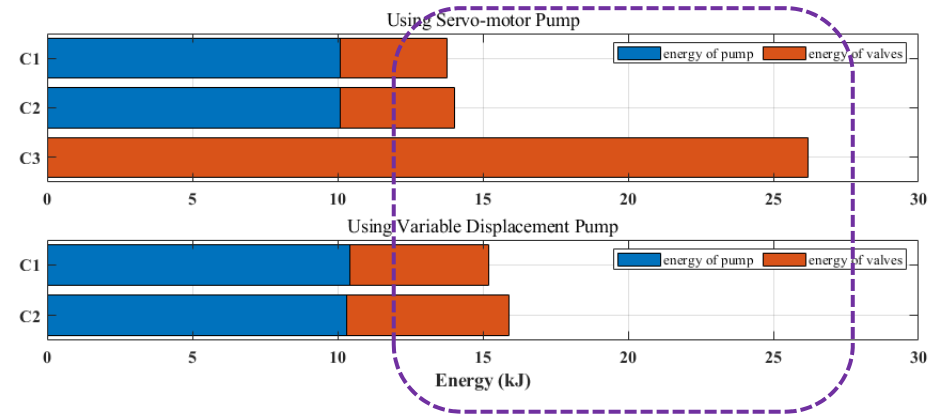
Comparative Experiments with Controller I

■ Energy consumption analyses

Accumulator pressure comparison



Energy calculation results



- ✓ **High level of energy efficiency:** both **C1** & **C2** (about 40%~50% less than **C3**)
C3: an energy efficient valve controlled system
- ✓ **C1** is a little better than **C2** (more obvious with the variable displacement pump due to the poor dynamic performance)

L. Lyu, Z. Chen and B. Yao, "Development of Pump and Valves Combined Hydraulic System for Both High Tracking Precision and High Energy Efficiency," in *IEEE Transactions on Industrial Electronics*, vol. 66, no. 9, pp. 7189-7198, Sept. 2019.

L. Lyu, Z. Chen and B. Yao, "Pump and Valves Coordinated System with Further Improved Energy Efficiency", Joint IFAC CAMS & WROCO, September 18-20, 2019, KAIST, Daejeon, Korea

Control Design I

- **High control performance & high energy efficiency**
- *Easy to implement in practice (feedforward control of the pump)*



What still can be improved?

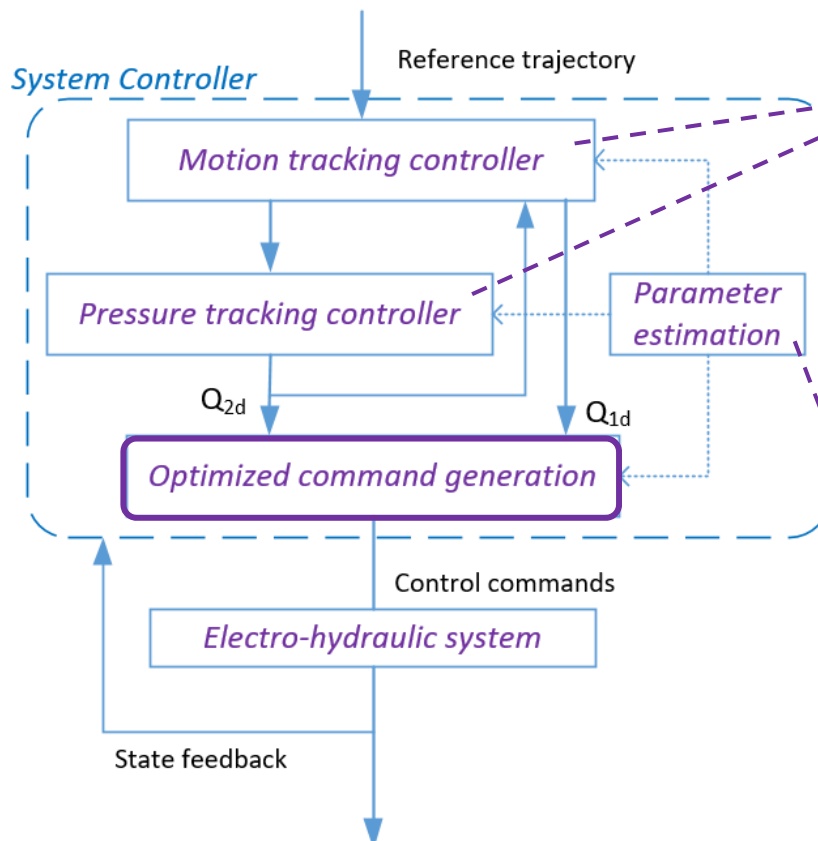
- A. discrepancies** between the desired one Q_{1d} & Q_{2d} and the ideal flow $Q_{1\text{ ideal}}$ & $Q_{2\text{ ideal}}$
 - will lead to extra energy wastes & cannot be reduced or minimized
- B. The pump is not “actively controlled”**
 - the control command has been decided once the reference trajectory is given
 - the pump would not adjust based on the real-time information about the system

How to minimize the throttling losses by controlling the pump actively?

Control Design II

- Same hardware configuration **using the servo-motor pump**

- Better** dynamic performance, but **still not as good as the valves**



- **Desired compensation integrated direct/indirect ARC (DCDIARC)**

- Desired cylinder flow Q_{1d} and Q_{2d}

- Desired states** ($x_d, \dot{x}_d...$) instead of the feedback signals in the model compensation terms

- Separated parameter estimation

Control Design II

■ Optimized command generation

-Desired cylinder flow Q_{1d} and Q_{2d} are given by the motion & pressure tracking controller

$$\begin{aligned}
 \underline{Q_{1d} = Q_{1da} + Q_{1ds}} \\
 Q_{1da} = Q_{1da1} + Q_{1da2} + Q_{1da3}, Q_{1ds} = Q_{1ds1} + Q_{1ds2} \\
 Q_{1da1} = \frac{V_{1d}}{A_1} \left[\left(\frac{A_1^2}{V_{1d}} + \frac{A_2^2}{V_{2d}} \right) \dot{x}_d - \frac{A_2}{V_{2d}} Q_{2da} - \frac{A_1}{V_{1d}} \hat{\theta}_7 - \frac{A_2}{V_{2d}} \hat{\theta}_8 \right. \\
 \left. + \left(\frac{\partial F_{Lda1}}{\partial t} + \frac{\partial F_{Lda1}}{\partial \hat{\theta}_{s1}} \dot{\hat{\theta}}_{s1} + \frac{\partial F_{Lda2}}{\partial t} \right) \hat{\theta}_5 \right] \\
 Q_{1da3} = -\frac{V_1}{A_1} \frac{A_2}{V_2} Q_{2ds} \quad Q_{1da2} = -\frac{V_{1d}}{A_1} \hat{d}_2 \\
 Q_{1ds1} = -k_{3s1} z_3, \quad Q_{1ds2} = -k_{3s2} z_3
 \end{aligned}
 \quad
 \begin{aligned}
 \underline{Q_{2d} = Q_{2da} + Q_{2ds}} \\
 Q_{2da} = Q_{2da1} + Q_{2da2}, Q_{2ds} = Q_{2ds1} + Q_{2ds2} \\
 Q_{2da1} = A_2 \dot{x}_d - \hat{\theta}_5 V_{2d} \dot{p}_{2d} - \hat{\theta}_8 \quad Q_{2da2} = V_{2d} \hat{d}_p \\
 Q_{2ds1} = -k_{ps1} z_p, \quad Q_{2ds2} = -k_{ps2} z_p
 \end{aligned}$$

Low-frequency terms (desired model compensation)---to generate **pump commands**

Q_{1da1}, Q_{1da2} & Q_{2da1}, Q_{2da2}

High-frequency terms (directly related to the **errors**)---to generate **valves commands**

$Q_{1da3}, Q_{1ds1}, Q_{1ds2}$ & Q_{2ds1}, Q_{2ds2}

■ Theoretical analyses

✓ Considering the **dynamic properties of the pump and the valves**

✓ **Optimized** to achieve high energy efficiency

-errors $\rightarrow 0$, valve flow $\rightarrow 0$, throttling losses $\rightarrow 0$

Comparative Experiments with Controller II

Tracking performance

-Set 1 low speed & Set 2 high speed

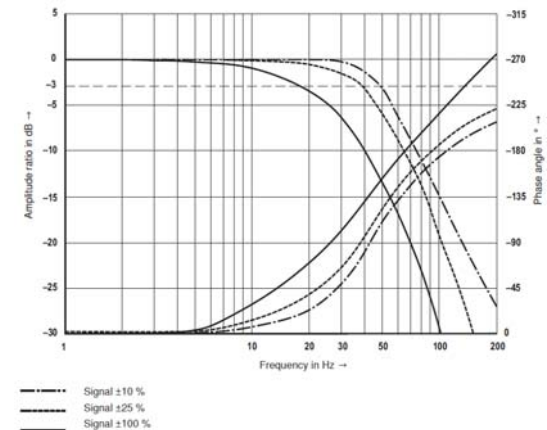
-C1: controller II C2: controller I using DCDIARC C3: four-valve independent metering

		$\ e\ _1 \cdot 10^{-3} m \cdot s$	$\ e\ _2 \cdot 10^{-6} m^2 \cdot s$	$\ e\ _{max} \cdot 10^{-3} m$
Set 1	C1	8.7	1.9	0.70
	C2	9.1	2.2	0.94
	C3	13.8	4.7	0.97
Set 2	C1	9.7	3.3	1.1
	C2	10.1	3.6	1.3
	C3	12.5	5.3	1.2

✓ C1, C2 & C3 achieved same level of high tracking performance

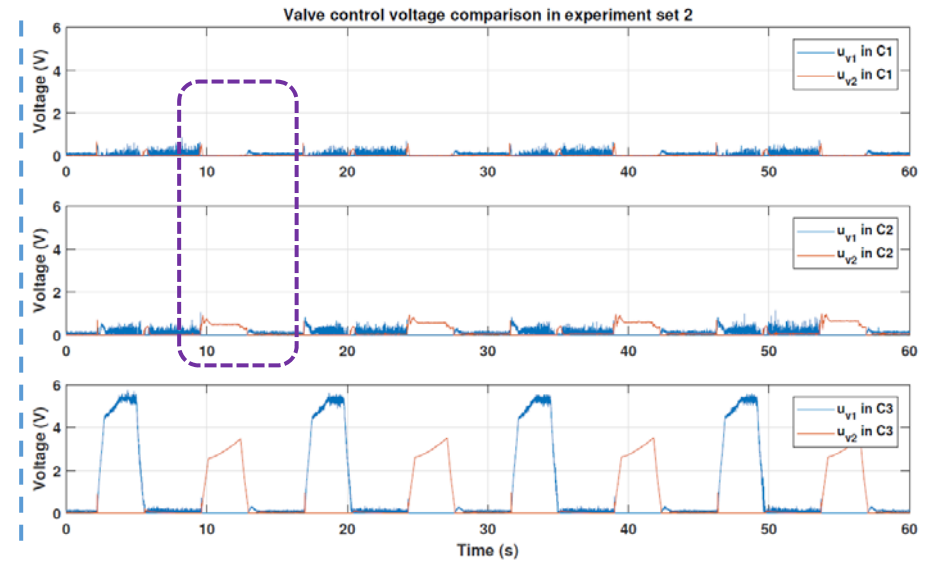
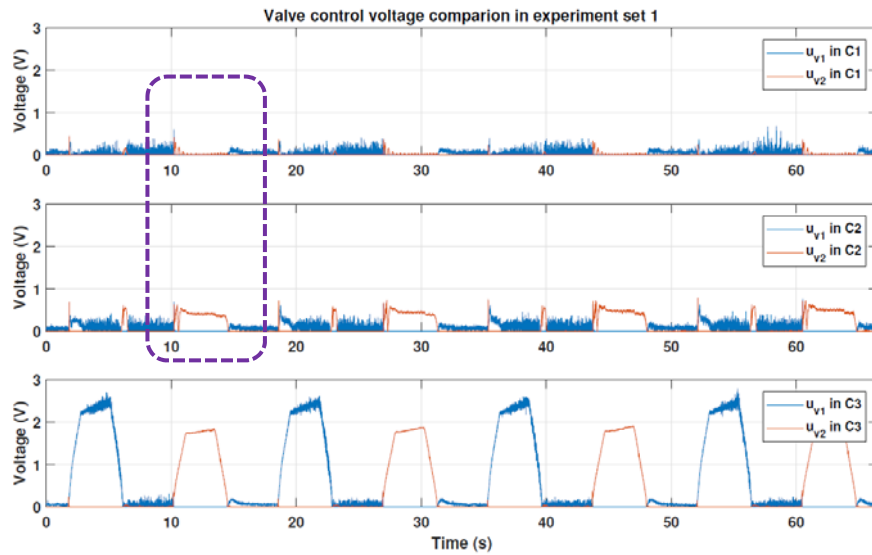
✓ Promising results: C1 even a little better than C3 (same valves)

higher available controller gains in C1 & C2:
small-signal range → higher bandwidth



Comparative Experiments with Controller II

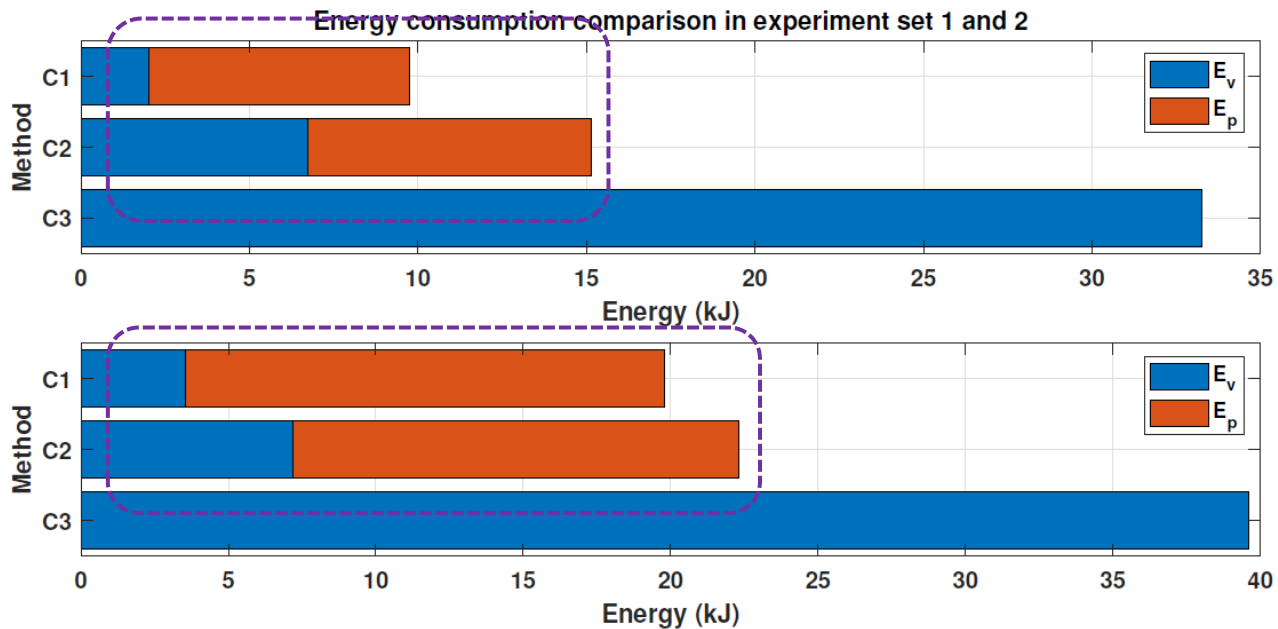
■ Control command comparison of the valves



- ✓ The control commands are within small-signal range in C1 & C2
- ✓ The control commands in C1 $\rightarrow 0$ --- optimized results, minimized throttling losses

Comparative Experiments with Controller II

■ Energy consumption comparison



- ✓ **Energy consumption C1** (about 50%~70% less than C3)
- ✓ **High level of energy efficiency: C1** (about 50%~70% less than C3)
- ✓ **Obvious energy saving effects** compared with controller I (about 14%~30% less than C2)

Conclusions

- **Brand new hardware configuration**

Parallel connection of the pump and independent metering valves

- **Control design I**

Easy to implement, feedforward control of the pump

- **Control design II**

Minimized throttling losses

High control performance & High energy efficiency

Thank You!